System Design: The Absentee in System Theory

Robert E Skelton UCSD June 2, 1999 ACC 619 822 1054, bobskelton@ucsd.edu

Dedicated to:

Osita Nwokah, Friend, Scholar

With a Little Help From My Friends

Adhikari Aldrich Callafon Grigoriadis Helton

Kiichiro Lu Mingori Murakami Pinaud Roman Sato Sultan Williamson Yamashita

Hubble Space Telescope (next servicing mission) • New Solar Array

Old Controller

Technology: What Paved the Way?

- 1st Half of 20th Century: **PHYSICS**
- 2nd Half of 20th Century: ENGINEERING

 (Component Technology)
 (Control is a component)

 Next? SYSTEMS

 (Interdisciplinary Technology)

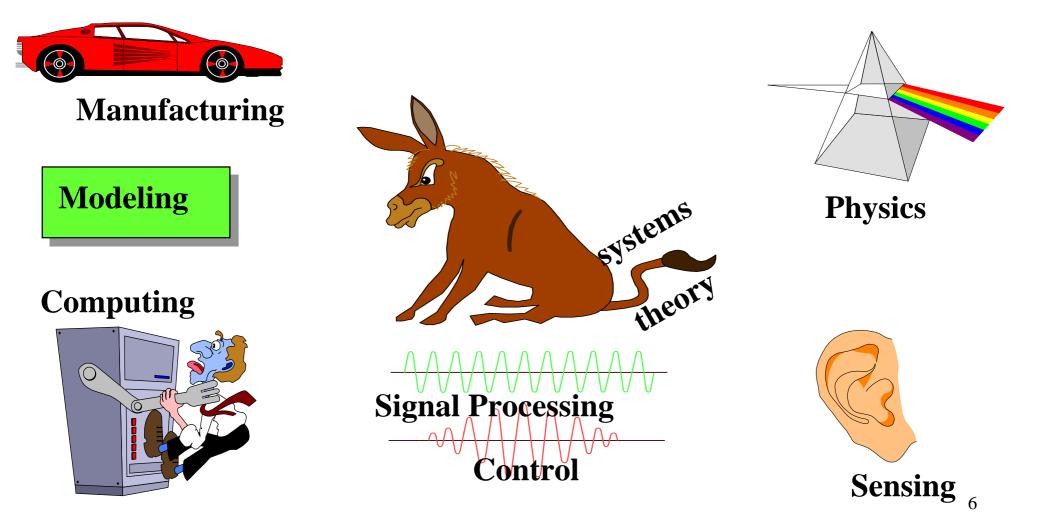
Outline

- Designing Systems
- Designing Models for Systems
- Inspirations From



Designing Controlled Structures

Pin the Tail on the Performance Limiting Technology



Systems Design Today

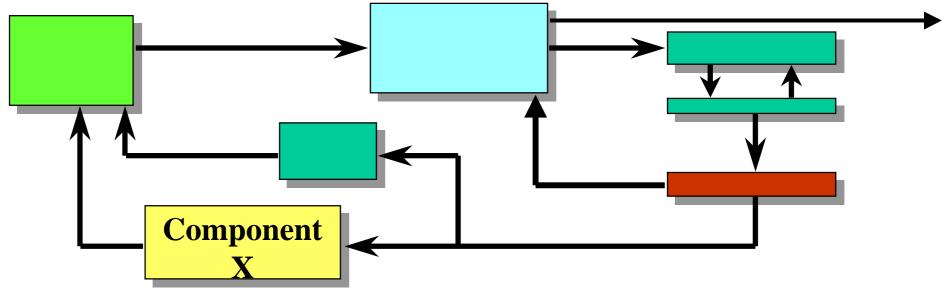
- Universities Teach Component Technology
 - materials, dynamics, signal processing, control
- Leading to: uncoordinated multidisciplinary tasks
 - Manufacture components, then
 - Model components (physics), then
 - Connect, Measure, Actuate components, then
 - Control the interconnected components
- Problem: dealing with sufficient rather than necessary
- Systems approach needed
- *Michael Faraday*: "Begin with the whole, then construct the parts"

When is the Whole LESS Than the Sum of the Parts?

- The answer: usually
- Today, components are overdesigned to compensate for the lack of coordination in their design
- A Misconception: "The best system is made from the best components"
- Often, more gain in integrating two disciplines, than gained by new technology in either discipline
- Examples

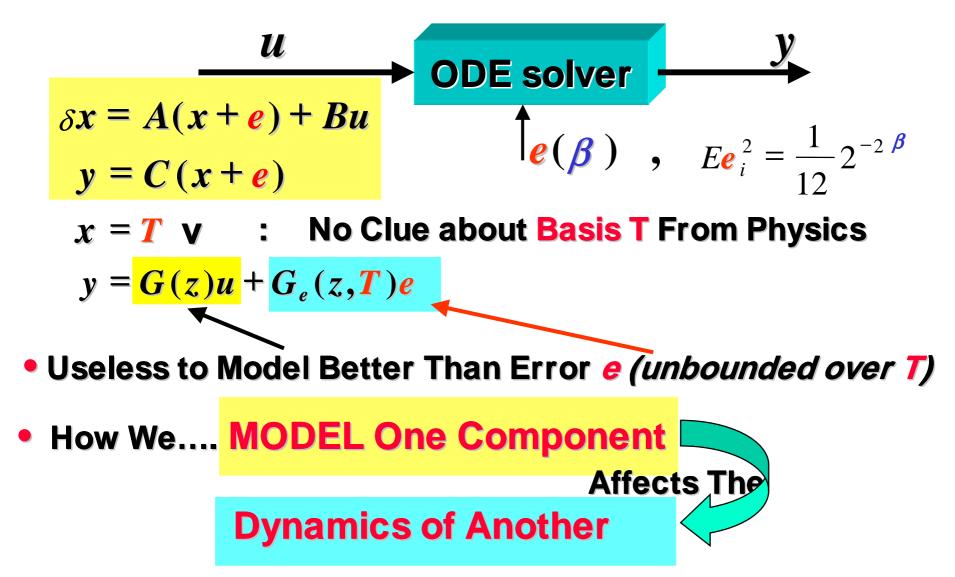
Given a System Requirement Where Should We Invest?

- How accurately to Model component X?
- How accurately to Manufacture component X?
- Is Component X even Necessary?
- How should the components be **Connected**?



Control is a Component technology

Finite Precision Computing



Unified Signal Processing/Control U **ODE solver** $\delta x = A(x + e) + Bu$ $|e(\beta)$, $Ee_i^2 = \frac{1}{12}2^{-2\beta}$ y = C(x + e)**No Clue about Basis T From Physics** x = T v $y = \frac{G(z)u}{G_e(z,T)e}$ $\min_{\mathbf{G}} \| G_e(\mathbf{T}) \boldsymbol{e}(\boldsymbol{\beta}) \|$ [Mullis/Roberts 76] [Williamson 86] [liu/Grigoriadis/Skelton 88] $\ni (\mathbf{T}^{-1}(\mathbf{Exx}^{T})\mathbf{T}^{-T})_{ii} = 1$ [Gevers 92, Bamieh 94] Component technology: Design (A,B,C), then T Systems technology: **Design (A,B,C,T) jointly** Control: Coupled ARE(β)

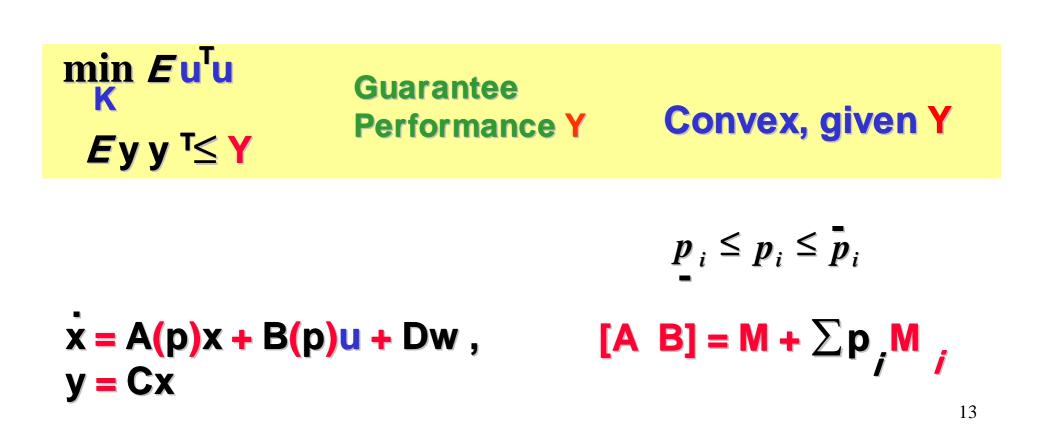
Hubble Space Telescope

Limited by control
Improvement @ no cost by unifying 2 disciplines

Using 24 bits: 100 times less (pointing variance)/(control energy) Using 4 bits: 10,000 times less (") change existing coefficients (no cost solution) IEEE TAC, Vol 37, No.9, 1992, JGCD, vol 18, No.2, 1995]

Optimal Mix of Plant/Control Design

[Grigoriadis, Zhu, Skelton, 1992]



Optimal Mix of Plant/Control Design

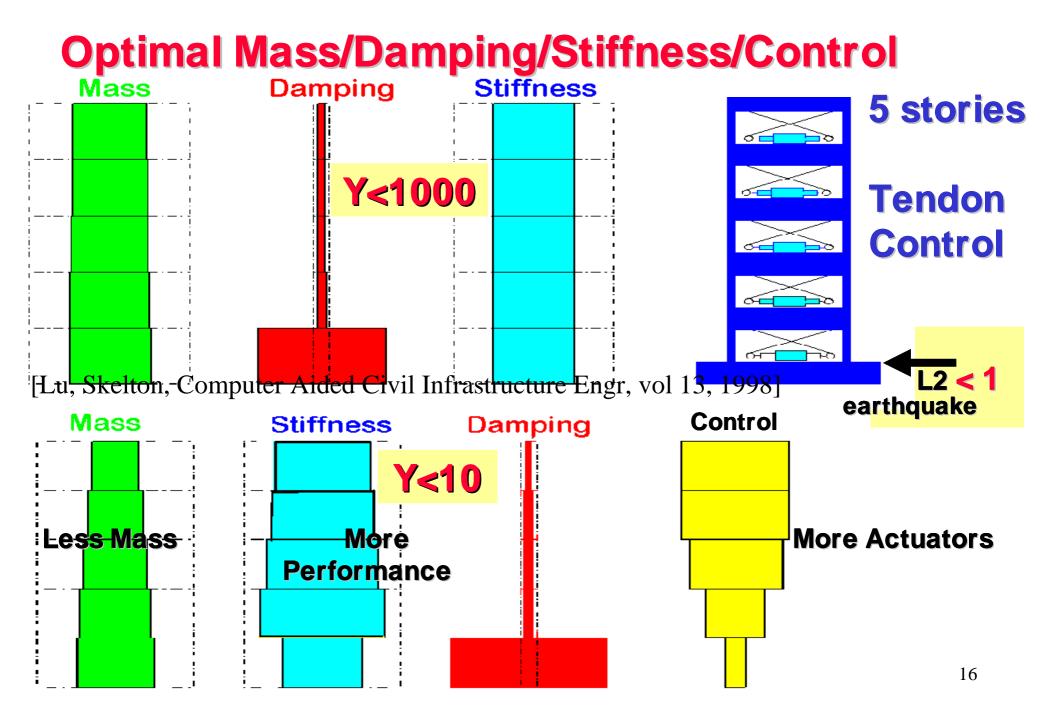
[Grigoriadis, Zhu, Skelton, 1992]

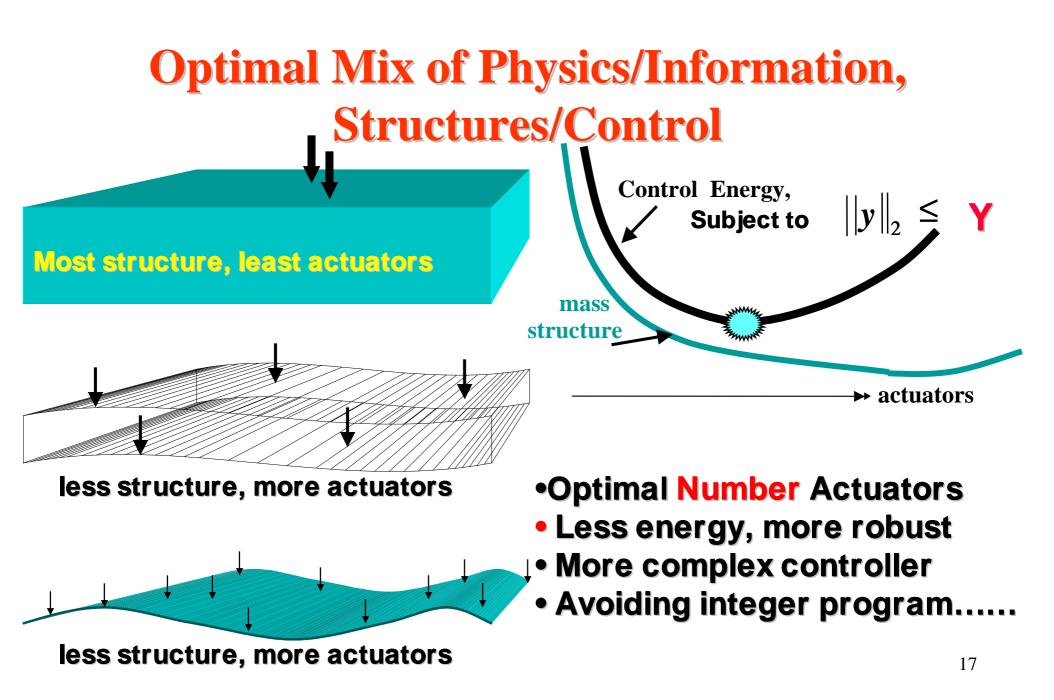
min Eu [™] u p, K Ey y [™] ≤Y	Update Plant p, Control K	Not Convex $p_i \leq p_i \leq p_i$
min Eu [⊤] u K Eyy [⊤] ≤ Y	Guarantee Performance Y	Convex, given Y

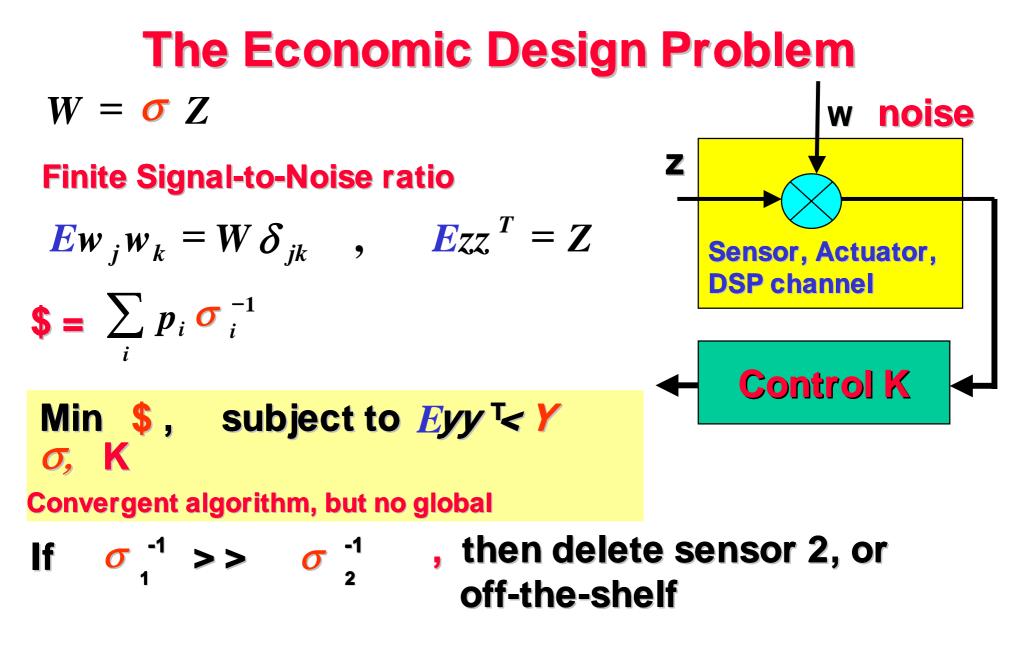
 $\dot{x} = A(p)x + B(p)u + Dw$, y = Cx

$$[A B] = M + \sum p_i M_i$$

Optimal Mix of Plant/Control Design [Grigoriadis, Zhu, Skelton, 1992] Euu min **Update** Convex, given X Plant p, $E \mathbf{X} \mathbf{X}^{\mathsf{T}} = \mathbf{X}$ $p_i \leq p_i \leq \bar{p}_i$ **Control** min **Eu^Tu** Guarantee **Convex, given Y Performance Y** *E* y y [™]≤ Y Compute $E xx^{T} = X$ where $CXC^{T} \leq Y$ X $[A B] = M + \sum p_{i}M_{i}$ x = A(p)x + B(p)u + Dw,y = Cx







[Lu, Skelton, Automatica, to appear]

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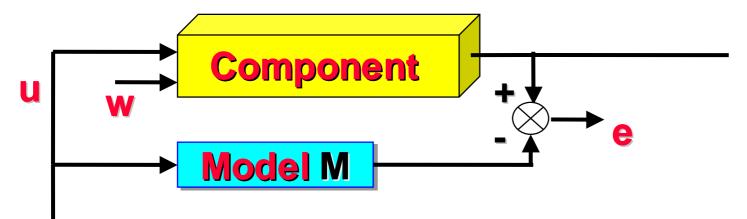




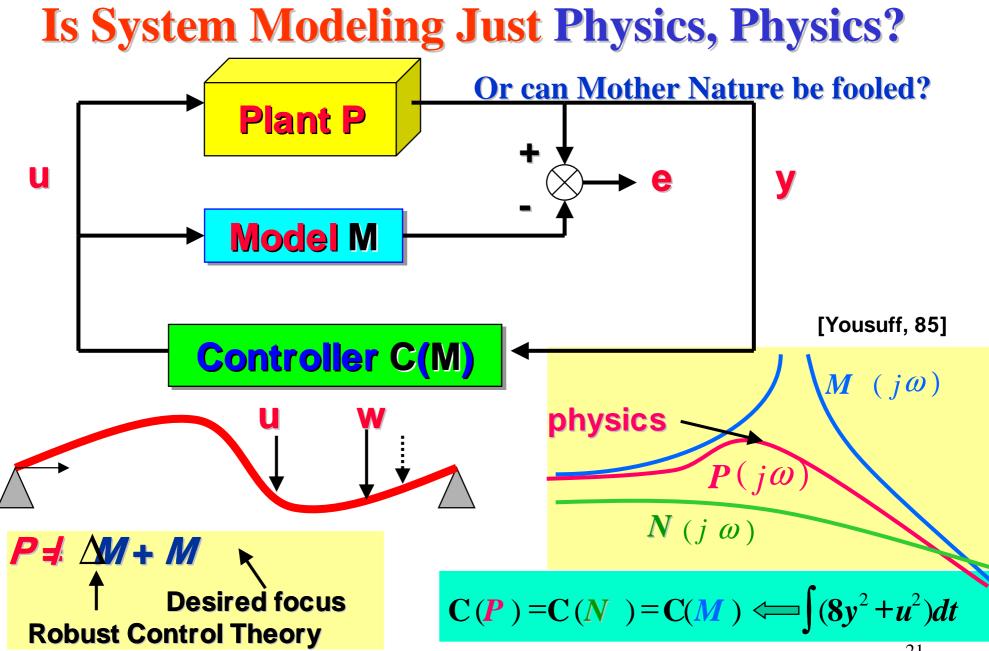
Designing Controlled Structures

Component Modeling

[Hu/Skelton, Computers and Structures, 1985]



•From physics, Choose Φ for small e •From systems criteria, $\mu(\zeta, t) = \Phi(\zeta) v(t) \leftarrow$ Choose Φ to depend on u,w recall $x = Tv \leftarrow$ Choose T to depend on w(b)



Control Models : How Much Info is Really *Minimize* $\sum_{k=1}^{N} (y_k^T Q y_k + u_k^T R u_k)$ **Necessary?**

Subject to $x_{k+1} = Ax_k + Bu_k$, $y_k = Cx_k$

[Shi, Skelton, DATA-BASED CONTROL, '94], [Furuta, '93], [Ikeda, '99]TheoremOptimalControllerRequires Only

 $CA^{i}B$, i = 0, 1, 2, ..., N - 1

Only Errors in CA ⁱ BAffect Control Performance
Any QMC from data yields the optimal control
Why compute Markov Parameters, Use Data Directly

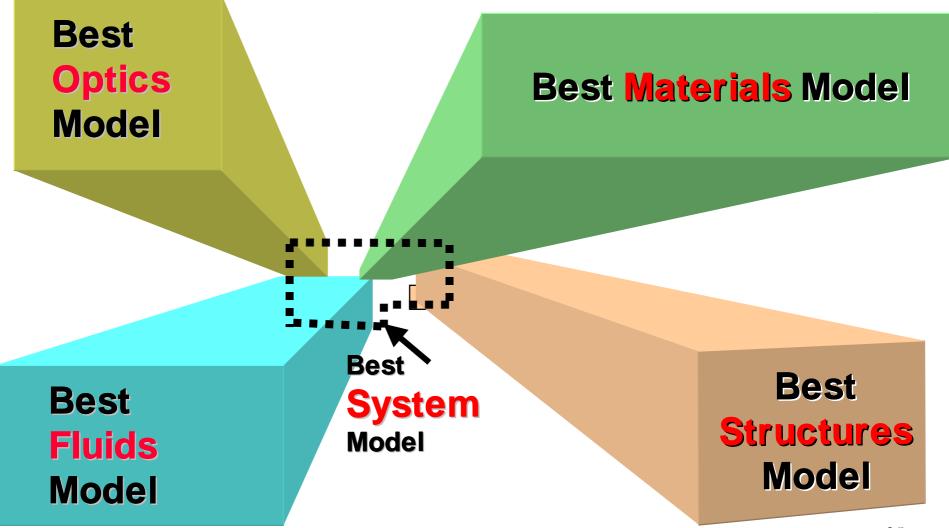
Data Equivalent Models [Skelton, Zhu, Qmarkov COVER, 1991] u Contraction of the second se **Does there exist any linear model to Match** the input/output data? $\mathsf{IFF} \qquad \mathbf{R} - \mathbf{H}\mathbf{H}^T \geq \mathbf{0}$ $\boldsymbol{R}_{i} = \boldsymbol{E}\boldsymbol{y}_{k+i}\boldsymbol{y}_{k}^{T}$, $\boldsymbol{H}_{i} = \boldsymbol{E}\boldsymbol{y}_{k+i}\boldsymbol{u}_{k}^{T}$ $\mathbf{R} = \begin{bmatrix} R_0 & R_1^T & R_2^T & R_3^T \\ R_1 & R_0 & R_1^T & R_2^T \\ R_2 & R_1 & R_0 & R_1^T \\ R_3 & R_2 & R_1 & R_0 \end{bmatrix}, \quad \mathbf{H} = \begin{bmatrix} H_0 & 0 & 0 & 0 \\ H_1 & H_0 & 0 & 0 \\ H_2 & H_1 & H_0 & 0 \\ H_3 & H_2 & H_1 & H_0 \end{bmatrix}$ Many Models Equivalent to the One From Physics

23

Absentee: A System Modeling Theory

- The size of the error is Not Continuous from Component (OL) to System (CL)
 - Unbounded OL error, but zero CL error
 - Smaller OL errors Smaller CL errors. Hence....
- Good Component Models Good System Models
 - There might exist a Better model for System Design than the Actual model from physics.
 - Bad News: Investments in Component Modeling may Not Help System Modeling
 - Good News: Good System Models can be Simpler Than Component Models (Yes, There Exists an Optimal Size)
- Should control design occur Before, After, or During plant modeling? 24

The Best System Model •May have little to do with the best **Component Model**



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 ART
 BIOLOGY
 - Designing Controlled Structures

Integrating Material, Structure, Control

- The Theory of Continua is inadequate to account for the strength of materials.
- Challenge for Man-made Systems: Architecture
 - Information Architecture: selection of sensors, actuators, and feedback paths.
 - Material Architecture: selection of the material geometry
- Look to Biological and Natural systems, where
 - Mechanical, Chemical, and Electrical forces are involved in complex patterns of information flow, sensing, and feedback

Inspiration From Art

After 30 Years of

- Forcing Continua
- Adding Actuators to Old Paradigms: Beams, Plates, Shells

Eureka !!!!

- •No Joints
- No Load Reversals
- No Friction
- •No Member Bending
- •Easy to Change Equilibrium

Kenneth Snelson Needle Tower, 1968 Kroller Muller Museum The Netherlands

"Tensegrity" = Tension + Integrity

Ingber, 98 Scientific American

Viennie lien

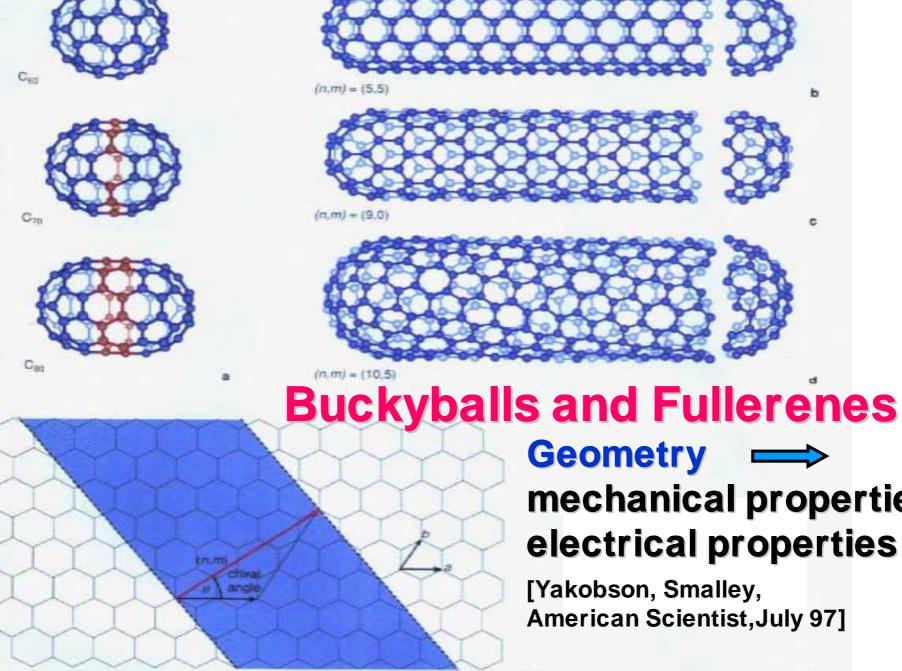
or loskalaion

Carbon Nanotubes, Fullerenes

Strength From Geometry

[Yakobson, Smalley, American Scientist, July 97]

Smalley, 1996 Nobel Prize



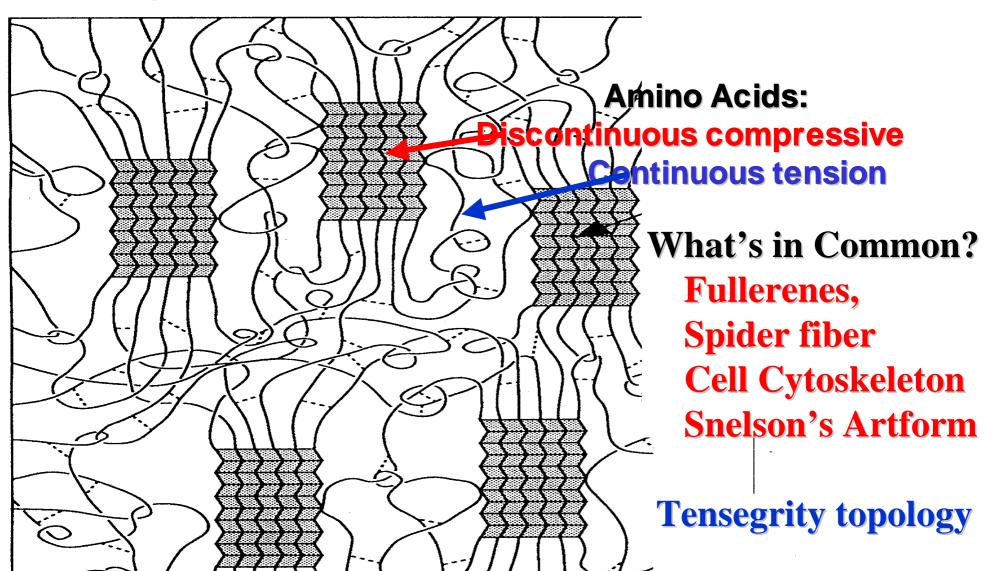
mechanical properties, electrical properties

C

[Yakobson, Smalley, **American Scientist, July 97]**

A Tensegrity Found in Nature,

Spider Fiber: Nature's Strongest



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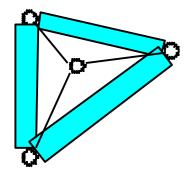


Designing Controlled Structures

Definition: Tensegrity Systems

2 N Points form a **Tensegrity Geometry** if the set of Points are stabilizable with pretensioned axially loaded members connecting the points, with no more than two compressive members attached to a Point

Class D: Discontinuous Compressive Members **Class C:** Continuous Compressive Members



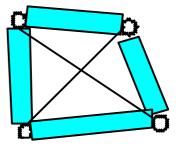
Tensegrity System

C3T3, Class C

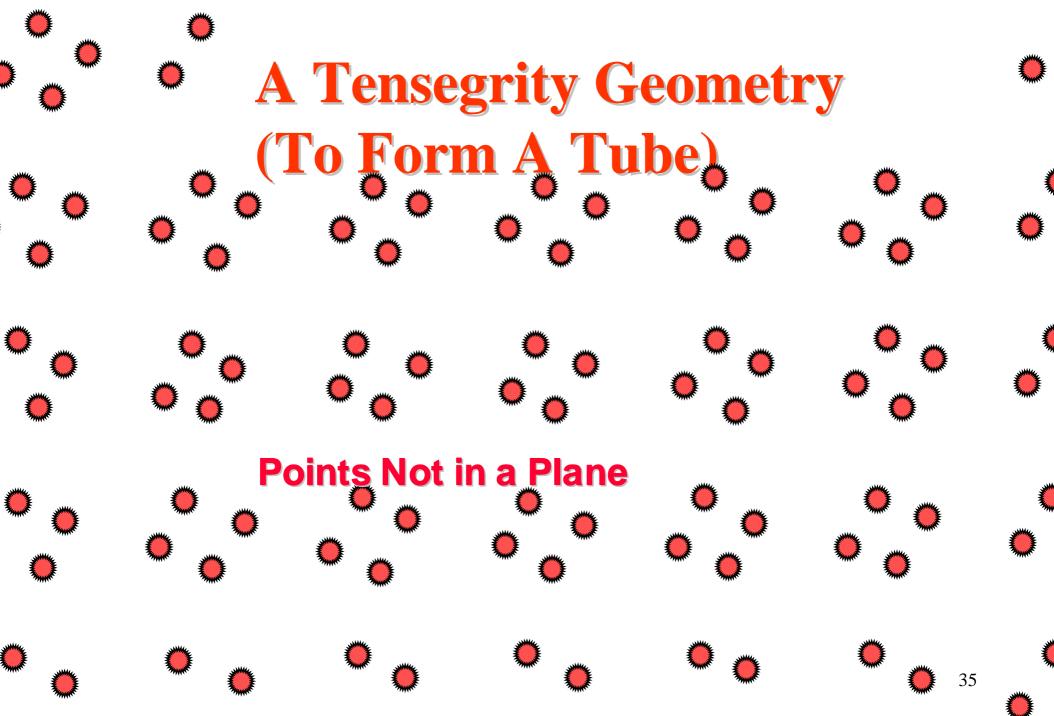
 t_1 t_4 t_4

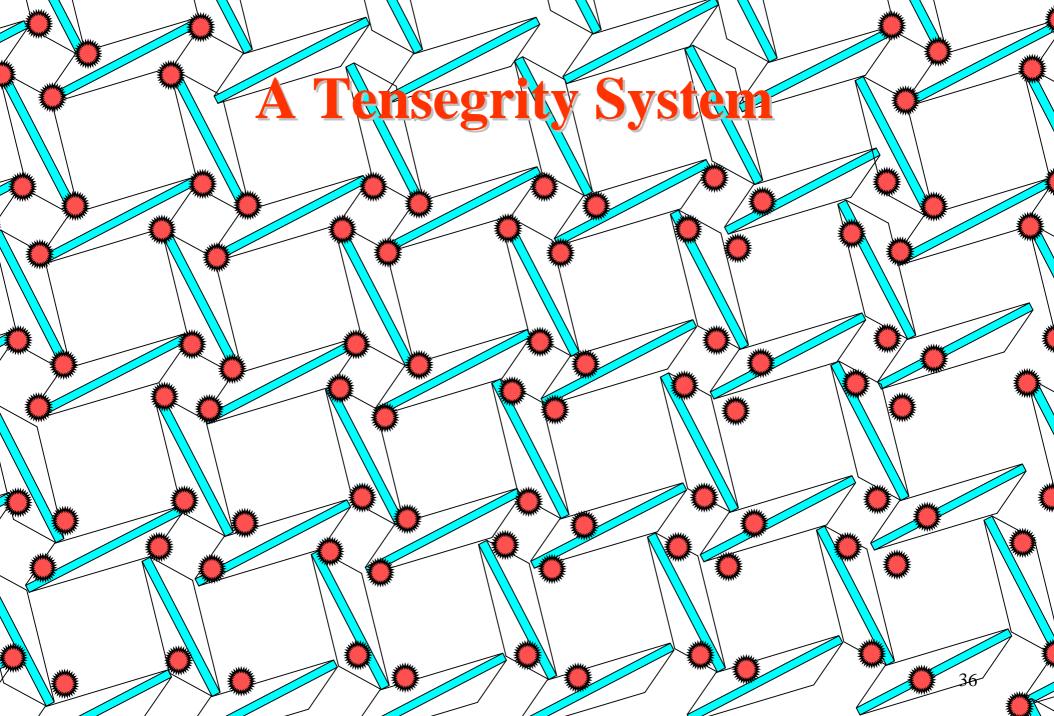
Tensegrity System

C2T4, Class D



3D: No Tensegrity



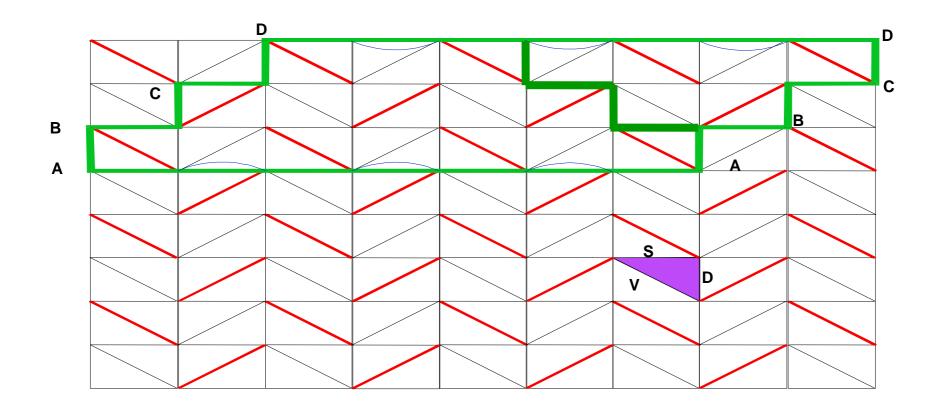


3 Local Parameters + Equilibrium Constraint

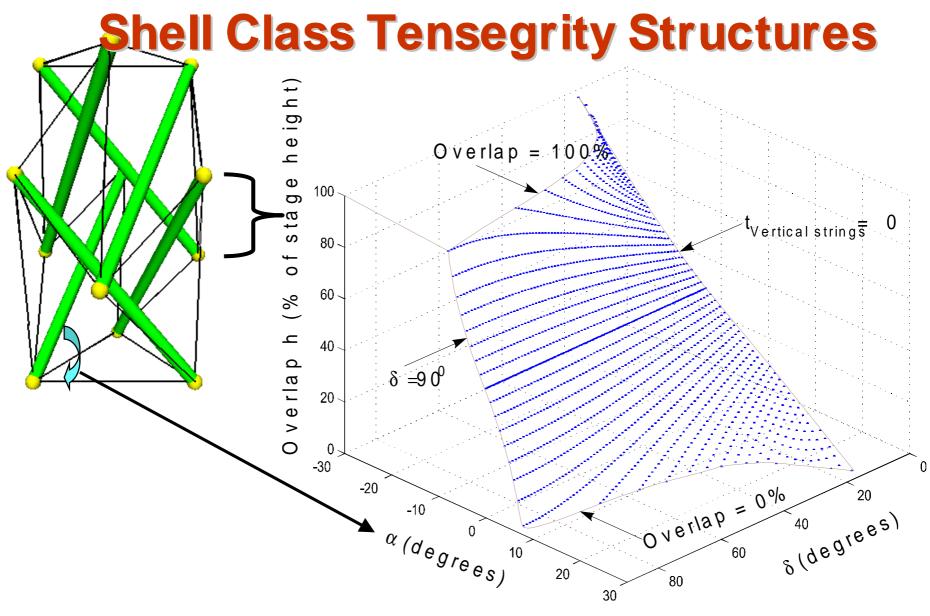
A Tensegrity System

Symmetric Geometry: 2 Free Parameters

Shell Class of Tensegrity Systems









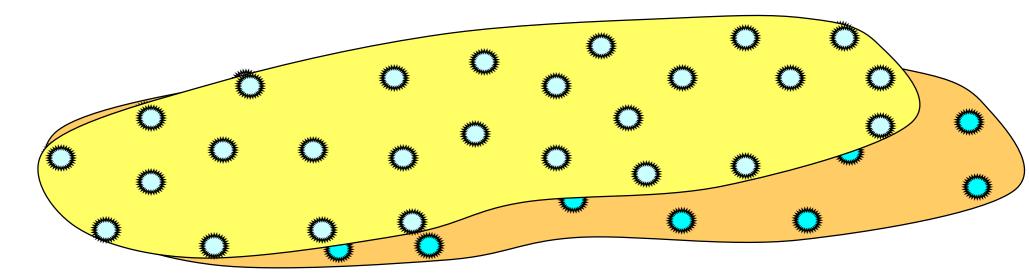
Structural Systems and Control Laboratory School of Engineering, UCSD

$$\begin{array}{ll} \textbf{Tensegrity Geometry} \\ (h, \alpha, \delta) &= \text{Stable equilibrium} \\ F(h, \alpha, \delta)t &= 0, \quad , \quad t > 0 \\ F^T F &= 0 \end{array} \right\} \begin{array}{l} \textbf{Tensegrity Geometry} \\ \textbf{Skelton, Helton, Adhikari, 1998],} \\ \textbf{h} &= \frac{1}{2 \tan \delta \cos \left(\alpha + \frac{\pi}{6}\right)} \\ \left(-\frac{L_L}{\sqrt{3}} + L \sin \delta \cos \left(\alpha + \frac{\pi}{6}\right) + \sqrt{\frac{L_L^2}{3} - 3L^2} \sin^{-2} \delta \cos^{-2} \left(\alpha + \frac{\pi}{6}\right)\right) \\ \textbf{Pugh, 1976} \\ \textbf{Pelligrino, Calladine, 1986} \qquad \textbf{Skelton, 1993 - 1999} \end{array}$$

Pelligrino, Calladine, 1986
Motro, 1986
Furuya, 1992
Coughlin, Stamenovic, 1997

Skelton, 1993 - 1999
Sultan, 1996,1997, 1998, 1999
Oppenheim, 1998
Williamson, Skelton, 1999

Tensegrity Paradigm for Structural Control



Changing the Shape With Less Control Energy
 Construct a Tensegrity Geometry with a specified shape
 Actuate the tendons (rest lengths) to avoid straining the structure, moving from one equilibrium to another

Shape Control with Tensegrity

Theorem [99] Let q1, q2 be two tensegrity geometries, associated with the same nullspace of F(q). Then, •There exists a continuum of tensegrity geometries between q1 and q2.

•There exist tendon controls to change the geometry from q1 to q2 without changing potential energy.

$$\ddot{q} + (K_r(\dot{q}) + K_p(q))q = B(q)(u + v) + Dw$$

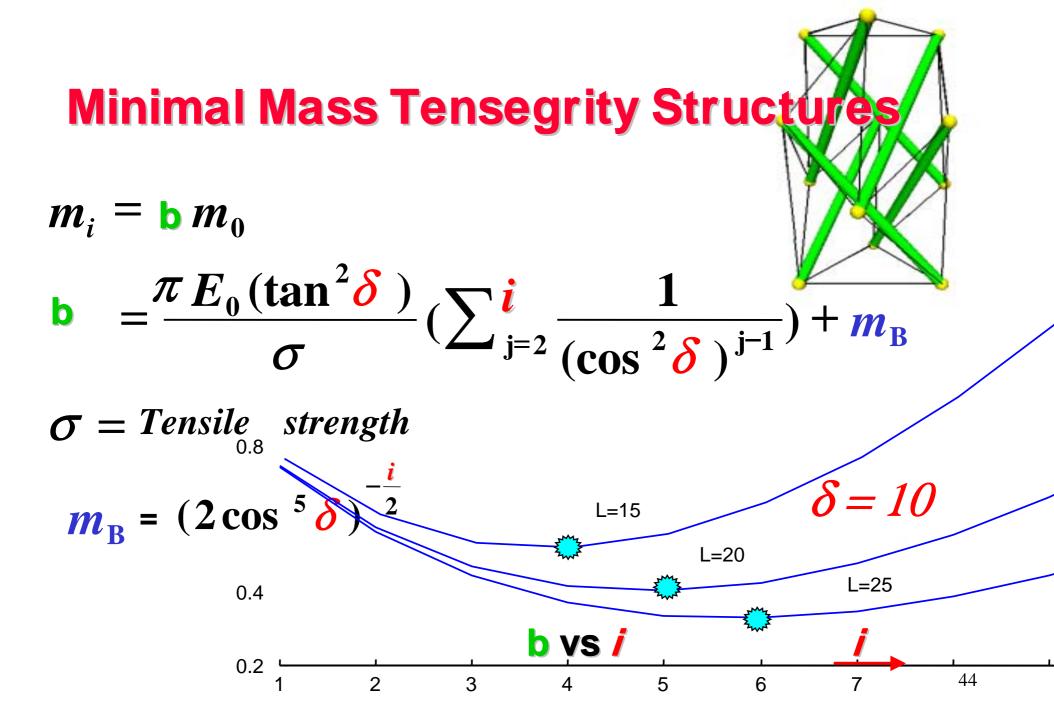
$$\dot{\boldsymbol{u}} = \boldsymbol{K}^{-1} (\boldsymbol{R}\boldsymbol{q} - \boldsymbol{u}) \frac{(\boldsymbol{R}\boldsymbol{q} - \boldsymbol{u})^T \boldsymbol{K}\boldsymbol{R} \, \dot{\boldsymbol{q}}}{(\boldsymbol{R}\boldsymbol{q} - \boldsymbol{u})^T (\boldsymbol{R}\boldsymbol{q} - \boldsymbol{u})} , \quad \boldsymbol{R}\boldsymbol{q} > \boldsymbol{u}$$

Controlling (Torturing) Structures

SMA torque tube

• Existing approach: (DARPA SMART WING)

- Design Control After Structure
- Twist the structure against it's equilibrium. This requires work (7 deg limit, 20 deg desired)
- New Paradigm: Unify at more fundamental level •Change shape by changing the equilibrium



Stiffness-to-Mass Ratio of C4T1ⁱ

Theorem

The compressive stiffness of the C4T1 Structure is equal to the tensile stiffness of the tendons of the shortest tendons

- Controlling the tension of the shortest tendon controls the compressive stiffness of the entire structure
- All compressive members carry the same load
- Infinite buckling strength for finite *i*
- minimal mass occurs at smaller *i* than infinite strength

Advantages of The Tensegrity Paradigm

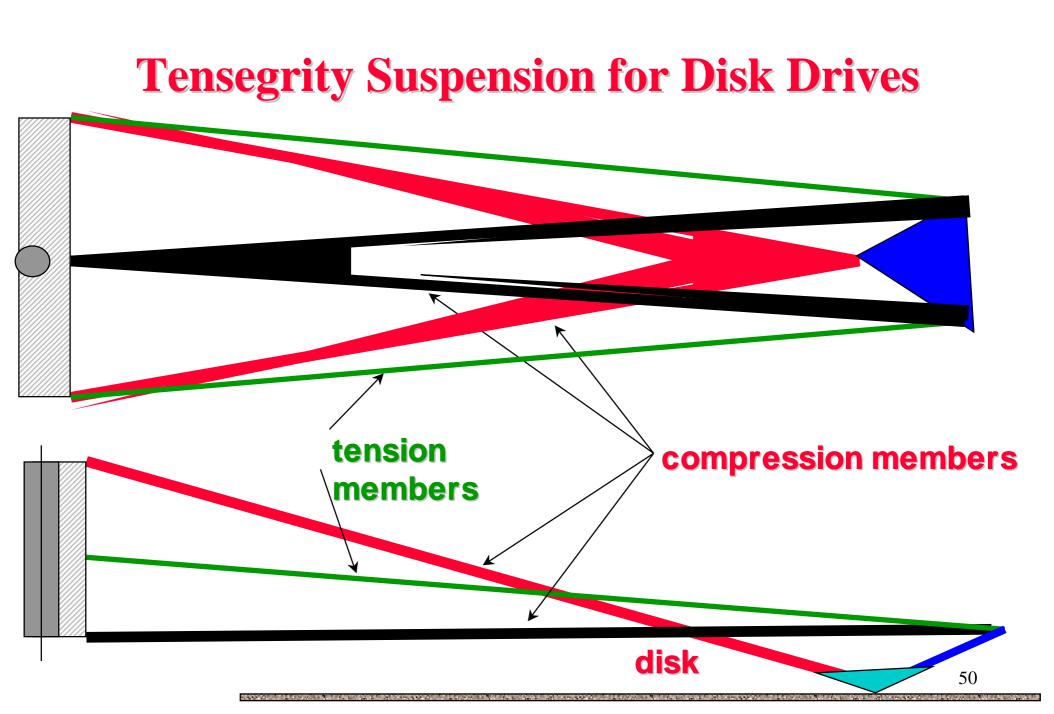
- All Members Axially Loaded
 - Global bending without member bending
- All Members Uni-Directionally Loaded (Pretension)
 - No reversal of load direction (no friction, hysteresis)
- Structural Efficiency
 - Strength to mass very high
 - Inspired by Art and Biological forms
- Easy to Integrate Structure/Control
 - More accurate models (hence more precise control)
 - A structural member also serves as sensor, actuator
 - Actuator/Sensor architecture easily optimized
 - Change shape with little work (one equilibrium to another)

Two-Stage Tensegrity: Tendon Control

Controlled tendons DC Motors



Single-Stage Tensegrity: Pneumatic



Conclusions

To Universities and funding agencies:

- Give the Soul of Control a Body: System Design
- Give Modeling a Purpose: Systems Modeling
- Function following Form
 - Snelson's Tensegrity Artform Inspires a New Paradigm to Integrate Mechanics, Structures, and Control

Conclusions

- After Component Technologies mature, the next quantum leap in technology must come from a scientific method to do Interdisciplinary System Design
- Why wait til component maturity to invest in a scientific method for Systems Design
- The biggest challenge: System Modeling
- System Design (and modeling) requires more than communicating what each discipline already knows
- We can exploit biological material architecture to
- Suggest a system design paradigm for designing to specific materials, thermal, electrical, mechanical properties:

What Your Data Never Told You

- Data is not Information
- Information is not Knowledge
- Knowledge is not Understanding
- Understanding is not Wisdom

[Howard Garner, Harvard]