

## Solutions Homework 3

1 If we don't neglect the movement of the free surface of the tank, the velocity at the surface is  $\mathbf{u} = \dot{h}\mathbf{e}_z$  and the potential in the tank can be taken to be  $\phi = \dot{h}z$ . If at the exit of the pipe,  $\mathbf{u} = U\mathbf{e}_x$  and the potential is  $\phi = Ux$  as in class, irrotational Bernoulli applied at the free surface and at the exit of the pipe gives

$$\ddot{h}h + \frac{1}{2}\dot{h}^2 + gh + \frac{p_0}{\rho} = \dot{U}L + \frac{1}{2}U^2 + \frac{p_0}{\rho}.$$

The velocities  $U$  and  $\dot{h}$  can be related using mass conservation by  $U = -(A/a)\dot{h}$  ( $\dot{h}$  is negative and  $U$  is positive).

Substituting into Bernoulli's equation, we get an equation for  $h$ :

$$\left(h + \frac{A}{a}L\right)\ddot{h} + \frac{1}{2}\left(1 - \frac{A^2}{a^2}\right)\dot{h}^2 + gh = 0.$$

The dimensional quantities in the problem are  $h, h_0, L, g, A, a$  and  $t$ . There are therefore a priori 5 independent nondimensional group. Write  $\beta = A/a$  and denote the scales for time and  $h$  by  $\tau$  and  $H$  respectively so that  $h = Hz$ . We obtain the equation

$$\left(z + \frac{\beta L}{H}\right)\ddot{z} + \frac{1}{2}(1 - \beta^2)z^2 + \frac{g\tau^2}{H}z = 0.$$

This leads us to pick  $H = L/\beta$  and  $\tau = \sqrt{gH}$ . This we can write down the equation with only the parameter  $\beta$  as

$$\ddot{z}(\beta^{-2}z + 1) + \frac{1}{2}(\beta^{-2} - 1)z^2 + z = 0$$

with initial condition  $z(0) = z_0 \equiv h_0a/LA$ .

This equation can be solved numerically, e.g. using MATLAB. Results are shown below. For large  $\beta$ , as in class, we can drop the  $\beta^{-2}$  terms: this gives the dashed curves which are a good approximation. The hyperbolic tangent solution from class corresponds in addition to replacing the  $z$  term by  $z_0$ : these are the dot-dash curves, which are not such a good approximation. Note that the actual solution oscillates forever; the curves below have been truncated when  $h = 0$ .

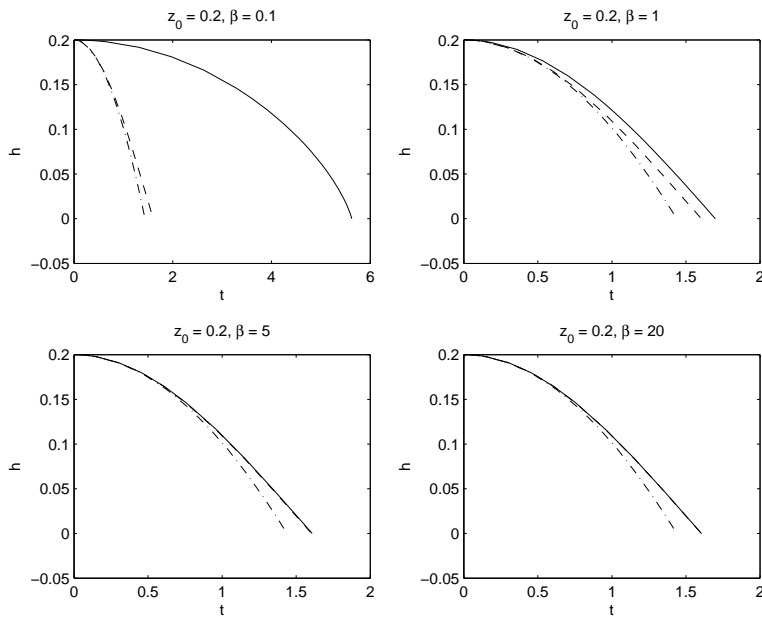


Figure 1:  $h(z)$  for  $z_0 = 0.2$ .

2 Assume incompressible inviscid flow. There are two possibilities: work either in the lab frame where the fluid has velocity  $\mathbf{u} = \Omega r \mathbf{e}_\theta$ , or in the rotating frame where the fluid is at rest but you need to add a centrifugal body force:  $\mathbf{f} = \Omega^2 r \mathbf{e}_r$ .

In the rotating frame, the fluid is at rest so  $\mathbf{u} = 0$ . The forces acting to a fluid particle are gravity, pressure and centrifugal force. Projecting the Euler equation along the radial, azimuthal and vertical axes gives

$$\begin{aligned} 0 &= -\frac{\partial p}{\partial r} + \rho \Omega^2 r, \\ 0 &= -\frac{\partial p}{\partial \theta}, \\ 0 &= -\frac{\partial p}{\partial z} - \rho g. \end{aligned}$$

Integrating this system gives  $p = p_0 + \frac{1}{2} \rho \Omega^2 r^2 - \rho g z$ .

Could you use Bernoulli? In the rotating frame, yes, because the body force is conservative and comes from a potential  $\mathbf{f} = -\nabla F$  with  $F = -\frac{1}{2} \Omega^2 r^2$ . You can use irrotational Bernoulli and therefore the Bernoulli function  $B = p/\rho - \frac{1}{2} \Omega^2 r^2 + \rho g z$  is a constant *everywhere* in the fluid.

If you stay in the lab frame, the flow is not irrotational anymore (solid body rotation) but steady. Steady Bernoulli would give you the same expression for

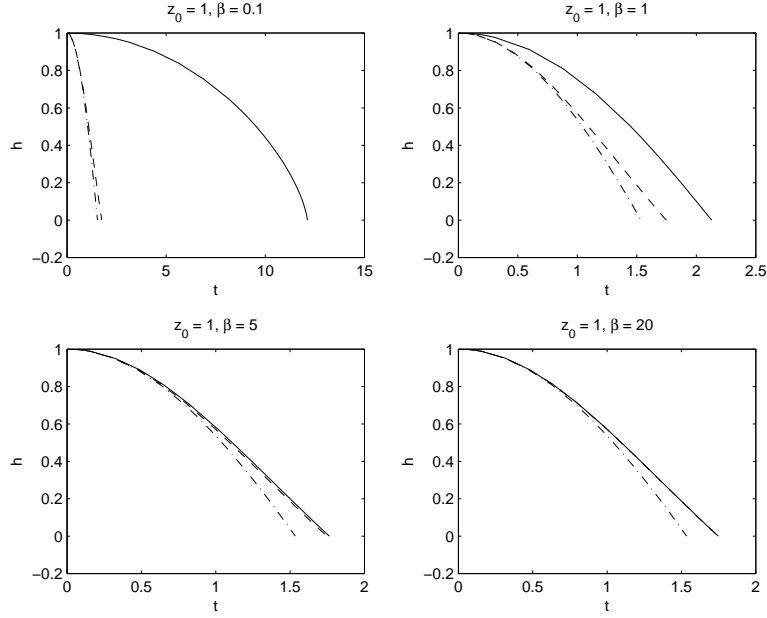


Figure 2:  $h(z)$  for  $z_0 = 1$ .

the Bernoulli function  $B$  but this time this function is only a constant along streamlines (circles around the vertical axis) and vorticity lines (vertical lines). Therefore  $B$  does not depend on  $z$  and  $\theta$ . But  $B$  is a function of  $r$ , and cannot be used to find the pressure everywhere.

The equation for the free surface is  $z = \zeta(r)$ . At the free surface, the boundary condition gives  $p = p_a$ . Therefore

$$p_a = p_0 + \frac{1}{2}\rho\Omega^2 r^2 - \rho g z.$$

Solving for  $\zeta$  gives

$$\zeta = \frac{\Omega^2 r^2}{2g} + \zeta_0,$$

where  $\zeta_0$  is a constant.

**3** Assume irrotational, inviscid and isothermal flow, and perfect gas. Then  $\mathbf{u} = \nabla\phi$  and  $p = \rho RT_0$ . The continuity equation can be written as

$$\frac{D \log \rho}{Dt} = \frac{1}{\rho} \frac{D\rho}{Dt} = -\nabla \cdot \mathbf{u} = -\nabla^2 \phi.$$

Unsteady Bernoulli gives

$$\frac{\partial \phi}{\partial t} + \frac{1}{2}(\nabla \phi)^2 + RT_0 \log \rho = 0,$$

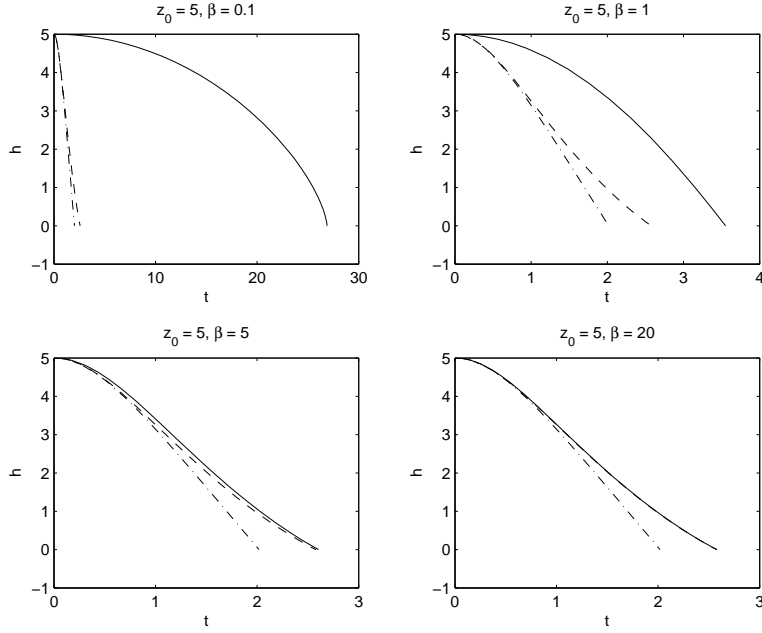


Figure 3:  $h(z)$  for  $z_0 = 5$ .

since  $\int dp/\rho = RT_0 \int d\rho/\rho = RT_0 \log \rho$ . The constant in the unsteady Bernoulli equation can be set to 0 without loss of generality.

Substituting for  $\log(\rho)$  in the continuity equation, we get an equation for  $\phi$  only

$$RT_0 \nabla^2 \phi = \frac{D}{Dt} \left( \frac{\partial \phi}{\partial t} + \frac{1}{2} (\nabla \phi)^2 \right)$$

which can be expanded if necessary into

$$RT_0 \nabla^2 \phi = \frac{\partial^2 \phi}{\partial t^2} + \frac{\partial}{\partial t} (\nabla \phi)^2 + \frac{1}{2} \nabla \phi \cdot \nabla ((\nabla \phi)^2).$$

If  $\phi = \Gamma \theta / 2\pi$ , the velocity is

$$\mathbf{u} = \nabla \phi = \frac{\Gamma}{2\pi r} \mathbf{e}_\theta.$$

Substituting this into the  $\phi$  equation shows that  $\Gamma$  must be constant in time. Substituting into the Bernoulli equation gives

$$\frac{\Gamma^2}{8\pi^2 r^2} + RT_0 \log p = C.$$

Applying the boundary condition at infinity gives

$$p = p_\infty e^{-\Gamma^2/(8\pi^2 RT_0 r^2)}.$$

For this isothermal compressible vortex, the pressure is zero at the center.

4 Start from the compressible form of the Euler equations in suffix notation

$$\frac{\partial u_k}{\partial t} + \frac{\partial}{\partial x_k} \left( \frac{1}{2} u_l u_l \right) + \epsilon_{klm} \omega_l u_m = -\frac{1}{\rho} \frac{\partial p}{\partial x_k} + \frac{\partial \Omega}{\partial x_k},$$

where  $\Omega$  is the potential for the conservative body force. The gradient terms disappear when we take the curl, but the pressure term doesn't since  $\rho$  is no longer constant. As shown in lectures,

$$\begin{aligned} [\nabla \times (\omega \times \mathbf{u})]_i &= \epsilon_{ijk} \frac{\partial}{\partial x_j} (\epsilon_{klm} \omega_l u_m) \\ &= \frac{\partial}{\partial x_j} (\omega_i u_j - \omega_j u_i) \\ &= (\mathbf{u} \cdot \nabla) \omega_i + (\nabla \cdot \mathbf{u}) \omega_i - (\omega \cdot \nabla) u_i. \end{aligned}$$

For the pressure term,

$$\begin{aligned} \epsilon_{ijk} \frac{\partial}{\partial x_j} \left( \frac{1}{\rho} \frac{\partial p}{\partial x_k} \right) &= -\frac{\epsilon_{ijk}}{\rho^2} \frac{\partial \rho}{\partial x_j} \frac{\partial p}{\partial x_k} + \epsilon_{ijk} \rho \frac{\partial^2 p}{\partial x_j \partial x_k} \\ &= -\left( \frac{\nabla \rho \times \nabla p}{\rho^2} \right)_i, \end{aligned}$$

since the last term cancels by symmetry. Substituting in the original equation gives in vector form

$$\frac{D\omega}{Dt} = (\omega \cdot \nabla) \mathbf{u} - (\nabla \cdot \mathbf{u}) \omega + \frac{\nabla \rho \times \nabla p}{\rho^2}.$$

By the product rule

$$\frac{D}{Dt} \frac{\omega}{\rho} = \frac{1}{\rho} \frac{D\omega}{Dt} - \frac{\omega}{\rho^2} \frac{D\rho}{Dt}.$$

but the continuity equation gives  $D\rho/Dt = -\rho(\nabla \cdot \mathbf{u})$ . Combining this with the previous result gives

$$\frac{D}{Dt} \frac{\omega}{\rho} = \left( \frac{\omega}{\rho} \cdot \nabla \right) \mathbf{u} + \frac{\nabla \rho \times \nabla p}{\rho^3}.$$

The second term  $\rho^{-2} \nabla \rho \times \nabla p$  creates vorticity when isopycnals and isobars are not aligned: it is the *baroclinic torque* or *rate of vorticity generation due to the baroclinicity of the flow*. For barotropic flow,  $p$  is a function of  $\rho$  only and the two gradients are aligned so the torque vanishes. We also see that in the absence of this term,  $\omega/\rho$  is transported like a line element.