

Force and Flow Transition in Plowed Granular Media

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We use plate drag to study the response of granular media to localized forcing as a function of volume fraction ϕ . A bifurcation in the force and flow occurs at the onset of dilatancy ϕ_c . Below ϕ_c rapid fluctuations in the drag force F_D are observed. Above ϕ_c fluctuations in F_D are periodic and increase in magnitude with ϕ . Velocity field measurements indicate that the bifurcation in F_D results from the formation of stable shear bands above ϕ_c which are created and destroyed periodically during drag. A friction-based wedge flow model captures the dynamics for $\phi > \phi_c$.

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Granular materials are fascinating because they can act like both fluids and solids [1]. Recent work has focused on the static problem of mechanical rigidity (jamming) in which the packing density ϕ (the ratio of solid to occupied volume [2]) is increased until grains crowd sufficiently to develop a finite yield stress [3]. Less work has explored the related process of “unjamming” [4] where initially jammed granular ensembles flow in response to forcing and where the initial packing density plays an important role: varying ϕ changes the local packing structure of grains which in turn affects the flow and force dynamics of the material response.

We are interested in granular media subject to localized forcing (for instance, from limbs and bodies during locomotion [5]). In general, granular systems sheared at the boundaries evolve to a steady state ϕ_c [6]: depending on initial ϕ , the medium compacts ($\phi < \phi_c$) or dilates ($\phi > \phi_c$) as $\phi \rightarrow \phi_c$. In contrast, localized forcing, realized by an intruder translating through an initially homogeneous medium [4,7] and viewed in the reference frame of the intruder, drives material only in the vicinity of the intruder toward ϕ_c while simultaneously advecting undisturbed media into the flowing region. The result is the repeated unjamming of “fresh” material and the possibility of complex spatiotemporal dynamics in and around the zone of disturbed material surrounding the intruder.

Here we drag a flat plate through initially homogeneous granular media at prepared ϕ to continuously drive the system away from ϕ_c and measure the resulting force and flow fields. As ϕ increases, the onset of shear dilatancy at ϕ_c drives a bifurcation in force dynamics and media flow. This bifurcation is governed by a complex spatiotemporal flow response associated with the stability (instability) of shear bands nucleated by the plow above (below) ϕ_c and their evolution in response to plow motion. A model of shear band evolution captures the oscillatory behavior above ϕ_c and suggests complex dynamics below ϕ_c .

Experiment. — Drag measurements, see Figs. 1(a) and 1(b), were performed in a $27 \times 86 \times 13$ cm³ bed of poly-

disperse 256 ± 44 μ m glass beads (Potters Industries; density $\rho = 2.51$ g cm⁻³). Similar effects to those described here were observed in other granular materials (see supplementary material[8]), including heterogeneous beach sand and poppy seeds. Air flow through the porous floor initially fluidized the medium and then a combination of air flow (below fluidization) and mechanical vibration generated the desired initial volume fraction ($0.579 < \phi < 0.619$). Air flow was turned off prior to testing, and volume fraction was determined from bed height images as $\phi = M/\rho Ah$, where M , A and h are the bed mass, area and height, respectively. A stepper motor and linear translation stage displaced a 3.9 cm wide by 0.3 cm thick steel plate submerged to a variable fixed depth $7.5 < d < 9.5$ cm over a distance of 50 cm at a constant speed of $v = 4$ cm s⁻¹.

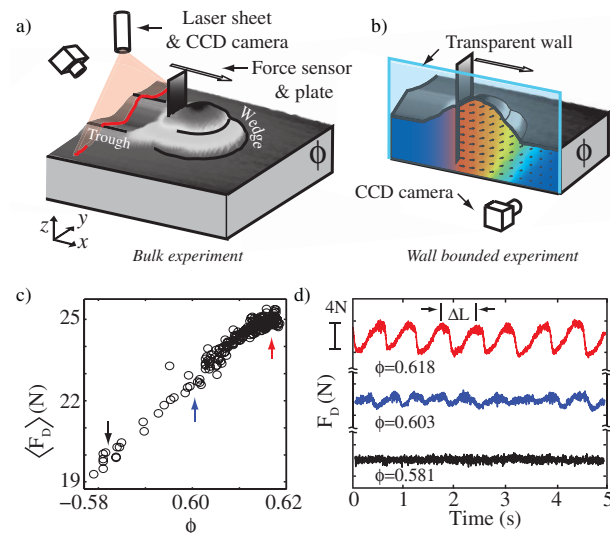


FIG. 1 (color online). Experimental overview. (a) Drag force, surface deformation, and (b) velocity fields are measured as a function of prepared volume fraction ϕ . (c) Mean drag force increases linearly with ϕ while (d) temporal fluctuations in F_D become periodic as ϕ is increased (arbitrary vertical shift).

An optical encoder recorded the position and a 3-axis load cell (ATI Industrial) mounted between plate and translation stage measured the drag forces (sampled at 200 Hz). Using laser line profilometry, we recorded the resultant surface profile and used it to quantify the change in vertical cross-sectional area, ΔA , normalizing by the submerged area of the plow, $A_p = \text{width} \times \text{depth}$. Profiles were measured 35 cm from the start of drag where the profile was in a steady state. In separate drag experiments a flat plate at depth $5.5 < d < 6.5$ cm was positioned against a transparent wall and displaced at $v = 2 \text{ cm s}^{-1}$ parallel to the wall to image grain flow. High speed video (250 frames per second) of the flow was recorded and analyzed in MATLAB using image registration with a correlation time step of 0.02 s [9]. The near-wall setup exhibited similar force fluctuations as the bulk but with approximately half the mean force. We remove two systematic variations in the force—a slow increase in the baseline force during drag ($\approx 5\%$ of the mean) and the decrease in depth of the constant height intruder with increasing ϕ —by defining the drag force F_D as the raw drag with slow drift removed (3rd order polynomial fit subtracted while preserving the mean) multiplied by a depth correction factor $(\frac{d_{LP}}{d})^2$ normalized to the loose pack depth d_{LP} . Separate measurements at controlled intruder depth support this normalization technique.

Force bifurcation.—The mean drag force increases approximately linearly with ϕ as expected due to increased bed density and average coordination number; see Fig. 1(c). A bifurcation, however, occurs in the force fluctuations: F_D at lower ϕ exhibits small amplitude, fast, and ϕ independent fluctuations. At higher ϕ , slower, periodic, and larger amplitude oscillations in F_D occur which grow in duration and magnitude as ϕ is increased [Fig. 1(d)].

We characterize the bifurcation by measuring the standard deviation of force σ_{F_D} and the average plow displacement between positive slope zero crossings of the force ΔL as a function of initial ϕ . As ϕ increases we observe a sharp bifurcation in σ_{F_D} and ΔL [Fig. 2(a)] at the dilation transition (i.e., $\Delta A/A_p = 0$ at $\phi_c = 0.603 \pm 0.003$); see Fig. 2(b). As the bifurcation is approached from below, σ_{F_D} is small and constant; above ϕ_c and with increasing ϕ , σ_F grows linearly while ΔL increases nearly linearly. For $\phi > \phi_c$, ΔL is independent of plow speed ($2 < v < 8 \text{ cm/s}$), see Fig. 2(a) inset, revealing it as a characteristic spatial scale and implying that the temporal dynamics of F_D result from granular flow mechanisms that change with ϕ across the dilation transition.

Flow bifurcation.—Direct evidence of a bifurcation in the flow is revealed by observations of the displacement of material at the surface near the plow [Fig. 3(a)]. Below ϕ_c surface deformation is smooth, and the boundary between upwardly moving grains and the undisturbed surface advances uniformly at a fixed distance ahead of the plow. At and above ϕ_c , however, the surface flow takes the form of

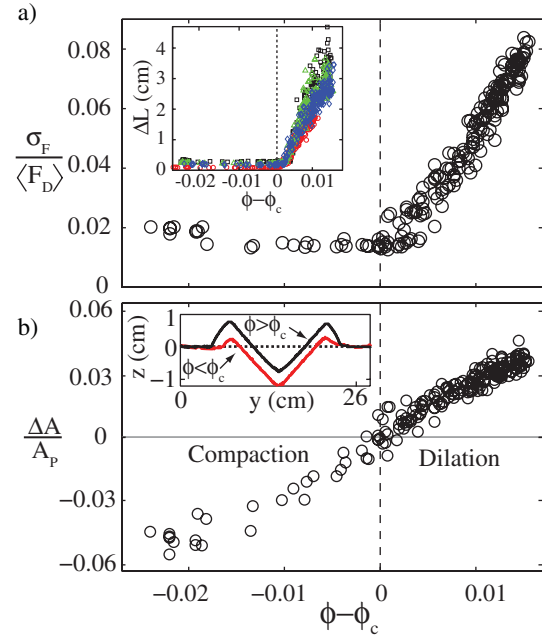


FIG. 2 (color online). Bifurcation in force occurs at the onset of dilation $\phi_c = 0.603 \pm 0.003$. Small and nearly constant for low ϕ , (a) standard deviation of F_D grows linearly above ϕ_c while (inset) force oscillation length scale increases nearly linearly ($v = 2, 4, 6, 8 \text{ cm s}^{-1}$ in red circles, blue diamonds, green triangles, and black squares). (b) Compacting and dilating response of plowed granular packings versus initial ϕ . Inset: Trough cross sections at high (black line) and low [gray (red) line] ϕ .

periodic radial upwellings of grains, which give the region around the plow a stepped appearance. The generation of surface ripples is correlated with fluctuations in F_D and indicates that the bifurcation in σ_{F_D} and ΔL results from a change in grain flow dynamics.

To gain insight into the nature of the bifurcation, we compare the grain velocity field at low and high ϕ in a vertical plane perpendicular to the displacement of the plow; see Fig. 3(b) and [8]. In both cases, flow is largely confined to a wedge-shaped region with angle θ in which grains move forward and upward in advance of the plow. At both values of ϕ a shear band separates the flowing wedge of grains and the effectively solidified grains outside the wedge; the lower end of the shear band originates at the bottom of the plate while the upper end terminates at the surface.

Temporal flow dynamics.—Despite these common features, significant differences in spatiotemporal evolution exist between flows at low and high ϕ . At low ϕ , flow is intermittent [Fig. 4(a)]: the horizontal extent of the flowing region η (measured at approximately half the intruder depth, 3.2 cm) rapidly advances and retreats as the plow moves into new material. At high ϕ , the spatiotemporal evolution of the flowing region is periodic with η remaining fixed for long periods of time until rapid, repeated fluctuations precede a jump forward to a new location.

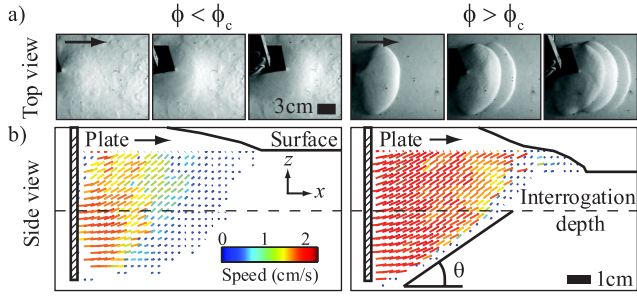


FIG. 3 (color online). Surface flow and velocity fields differ below ϕ_c (left) and above ϕ_c (right). (a) Surface deformation from a submerged plate shows steplike features above ϕ_c . (b) Snapshots showing differences in velocity field structure from transparent wall experiments [Fig. 1(b)].

We quantify the pinning of this flow boundary as the fraction of time η remains stationary ($\frac{d\eta}{dt} = 0$) during the entire drag. As ϕ increases η becomes increasingly stationary, indicating that the spatial shear regions are more stable. Above $\phi \approx \phi_c$, the shear band remains stationary for more than 50% of the drag duration.

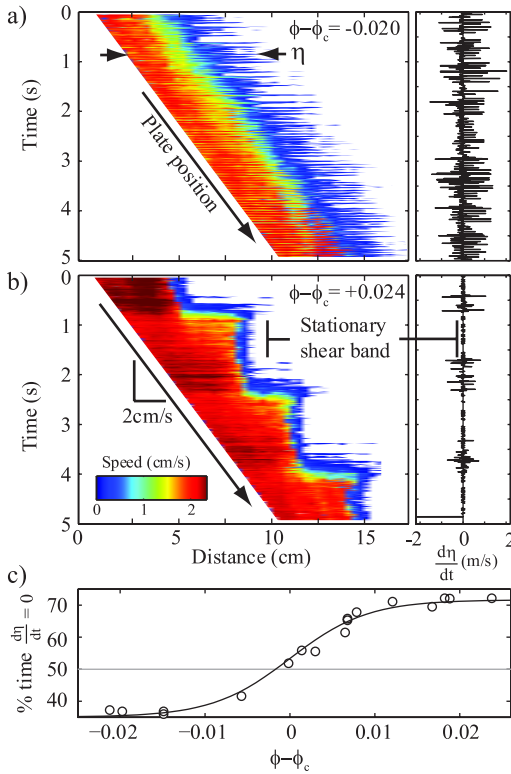


FIG. 4 (color online). Temporal evolution of flow differs below and above ϕ_c . Left: Space-time plots of flow speed along a constant depth horizontal strip show that the leading edge of the flow region η (a) fluctuates in loose pack and (b) is stationary between shear band formation events (four shown) in close pack. Right: Time series of $d\eta/dt$ highlight changes in stability. (c) Percentage of time during 5 s drag that the flowing region is stationary ($d\eta/dt = 0$) increases with ϕ and is fit to $[1 + e^{-(\phi - \phi_c)}]^{-1}$.

Shear zone localization can be understood by the process of granular shear weakening or strengthening. Below ϕ_c material compacts and strengthens under shear, continually frustrating the development of fixed shear zones and forcing shear to occur along a constantly changing set of failure surfaces. Above ϕ_c , however, material dilates and weakens under shear, causing flow to localize along a fixed plane. In a plowed system, shear localization for initial $\phi > \phi_c$ holds only shortly after shear band formation: as the plow advances into undisturbed material the shear band is forced to adjust. Using the average angle of the flow boundary θ to characterize the orientation of the shear zone [see Fig. 3(b)], we find that below ϕ_c force and flow are largely uncorrelated while above ϕ_c , θ and F_D are strongly correlated with F_D and θ increasing in concert; see examples in Fig. 5(a).

Wedge flow model.—We develop a model based on the correlation of F_D and θ to gain insight into the dependence of F_D on the flow state and ϕ . As the bottom of the shear

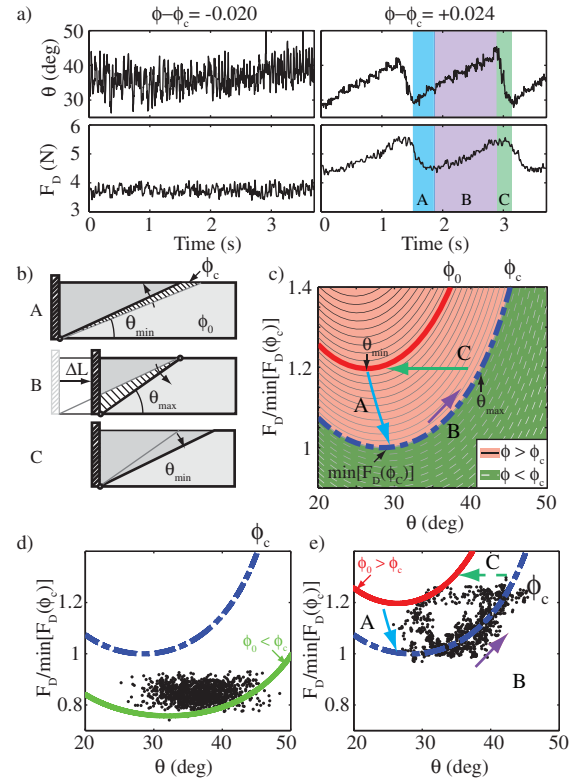


FIG. 5 (color online). Force dynamics and wedge model of granular flow. (a) Wedge flow angle θ and F_D are correlated above ϕ_c . (b) Sketch of wedge flow model dynamics above ϕ_c with arrows indicating motion of shear band for the three phases A, B, C also shown in (a), (c), and (e). (c) Dynamics predicted by model (arrows) showing family of (θ, F_D) curves for varying $\mu(\phi)$ and transitions between $\mu(\phi)$ curves corresponding to ϕ_0 (solid red curve) and ϕ_c (dash-dotted blue curve); see text. Comparison of model (θ, F_D) curves and experiment: (d) for $\phi < \phi_c$ experimental data are bounded by model curves of arbitrary $\mu < \mu(\phi_c)$; (e) for $\phi > \phi_c$ model shows good agreement with experiment.

zone is pinned to the bottom of the plow, the flowing region is taken to be a triangular wedge of mass $m = \frac{\rho W d^2}{2 \tan \theta}$ sliding up a plane inclined at angle θ . Kinetic friction between the wedge and plane, $\mu(\phi)$, is assumed to increase with ϕ . Balancing the forces from the plow (assumed horizontal), gravity, and sliding friction, the model predicts the plowing force $F(\theta, \mu) = \frac{\rho W d^2}{2} \frac{1 + \mu / \tan \theta}{1 - \mu \tan \theta}$, where W is the plow width [Fig. 5(c)]. The plowing force diverges at $\theta = 0$ (infinite block) and $\theta = \tan^{-1}(\mu^{-1})$ and is minimum at $\theta_{\min} = \tan^{-1}(\sqrt{\mu^2 + 1} - \mu)$. θ_{\min} decreases and $F(\theta_{\min})$ increases with increasing $\mu(\phi)$.

The model predicts that an initially jammed and homogeneous material with volume fraction ϕ_0 shears at an angle θ_{\min} when the force reaches $F_{\min}(\mu)$; see Figs. 5(b) and 5(c). For $\phi_0 > \phi_c$, shearing along the slip plane dilates and weakens the material locally, causing $\mu(\phi_0)$ to decrease to $\mu(\phi_c)$, which reduces F_D and slightly increases θ ; see path A in Fig. 5(c). As the plow advances, the angle of the weakened shear zone gradually increases along $F[\theta, \mu(\phi_c)]$, indicated by path B. The shear band remains fixed at the surface (causing θ to increase) instead of advancing with a constant angle because, evidently, less high ϕ material needs to be broken in the former case. With increasing θ , the force to push the wedge θ_{\max} eventually equals the force required to break the stronger material at $\phi_0 > \phi_c$, i.e., $F[\theta_{\max}, \mu(\phi_c)] = F[\theta_{\min}, \mu(\phi_0)]$. At this point a new shear zone forms in front of the plow, decreasing θ to $\theta_{\min}(\phi_0)$, and the cycle repeats (path C).

The dynamics observed in the experiment for $\phi > \phi_c$ are captured by the model as seen in $[\theta, F(\theta)]$ space [Fig. 5(e) and [8]]. Here the system evolves between two curves [$\mu = 0.65$ (dash-dotted blue curve) and $\mu = 0.78$ (solid red curve)] and the transitions between these states qualitatively match the predictions of our model. The model predicts the increase in force fluctuations with increasing ϕ above ϕ_c . However, for $\phi < \phi_c$ the evolution of F_D with θ is more complicated because of the lack of stability of the sheared regions through shear strengthening. As we assume a feedback process exists between the flow dynamics and F_D , strengthening of the material during shear results in the relocation of the shear band to a weaker region in the surrounding bulk. With the continuous advection of undisturbed weaker material and the heterogeneity in ϕ in the previously sheared region, predicting the shear process below ϕ_c is more challenging.

In summary, we observe a flow and force bifurcation in localized granular drag which occurs at the onset of dila-

tancy. Localized forcing in granular media induces a heterogeneous ϕ distribution in the region of flow and represents a new way to test theories of granular flow [10]. Previous studies of drag in granular media [7] were performed at slow speed to observe stick-slip fluctuations over distances on the order of a grain diameter; the effects of varying initial ϕ were not investigated. Our observations of a bifurcation as a function of ϕ support the findings of Schröter *et al.* [11] who reported a transition in dynamics at $\phi = 0.598$, and our measured ϕ_c is similar to that reported ($\phi_c = 0.591$) in recent impact experiments [12]. It is known that ϕ_c is a function of the applied stresses and cohesive or frictional interactions between the grains [6,13] so we do not place importance on the specific value.

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- [1] B. H. M. Jaeger, S. R. Nagel, and R. Behringer, *Rev. Mod. Phys.* **68**, 1259 (1996).
 - [2] R. Nedderman, *Statics and Kinematics of Granular Materials* (Cambridge University Press, Cambridge, England, 1992).
 - [3] A. Liu and S. Nagel, *Annu. Rev. Condens. Matter Phys.* **1**, 347 (2010).
 - [4] R. Candelier and O. Dauchot, *Phys. Rev. Lett.* **103**, 128001 (2009); M. Shaejabi, T. Unger, and J. Kertész, *Phys. Rev. E* **78**, 011308 (2008); J. Geng *et al.*, *Phys. Rev. Lett.* **87**, 035506 (2001); L. Silbert, A. Liu, and S. Nagel, *Phys. Rev. E* **73**, 041304 (2006).
 - [5] N. Mazouchova *et al.*, *Biol. Lett.* **6**, 398 (2010); C. Li *et al.*, *Proc. Natl. Acad. Sci. U.S.A.* **106**, 3029 (2009); R. Maladen *et al.*, *Science* **325**, 314 (2009).
 - [6] A. Schofield and C. Wroth, *Critical State Soil Mechanics* (McGraw-Hill, New York, 1968).
 - [7] I. Albert *et al.*, *Phys. Rev. Lett.* **84**, 5122 (2000).
 - [8] See supplementary material at <http://link.aps.org/supplemental/10.1103/PhysRevLett.105.128301> for videos from experiment and model.
 - [9] M. Guizar-Sicairos, S. Thurman, and J. Fienup, *Opt. Lett.* **33**, 156 (2008).
 - [10] G. MiDi, *Eur. Phys. J. E* **14**, 341 (2004); P. Schall and M. van Hecke, *Annu. Rev. Fluid Mech.* **42**, 67 (2010).
 - [11] M. Schröter *et al.*, *Europhys. Lett.* **78**, 44 004 (2007).
 - [12] P. Umbanhowar and D. Goldman, *Phys. Rev. E* **82**, 010301 (R) (2010).
 - [13] S. Fazekas, J. Torok, and J. Kertész, *Phys. Rev. E* **75**, 011302 (2007).